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Enhancement of Loadability Limit of Deregulated Power System via Adaptive Real-Coded Biogeography-Based Optimization

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ABSTRACT

Background: With the growing demand for power in the open market, the augmentation of TTC (total transfer capability) is one solution close at hand. **Objective:** This paper proposes an algorithm, based on adaptive real-coded biogeography-based optimization (ARCBBO), to determine the optimal location and capacity of FACTS devices such as thyristor-controlled series capacitor and static VAR compensator to increase the loadability and boost power transfer capability of the system. This problem has been considered as an optimal power flow (OPF) based enhancement of total transfer capability. Experiments were performed without and with FACTS devices. The proposed technique aims to improve the searching ability, enhance population diversity and maintain smooth convergence characteristics by using adaptive Gaussian mutation. **Results:** The proposed algorithm has been tested on standard 30-bus and IEEE 118-bus systems and outcomes compared with those of existing population-based methods. **Conclusion:** The solution quality of the proposed method is superior over other techniques reported in recent literature. Due to its simple framework, and smooth and quick convergence characteristics, the ARCBBO algorithm is suggested to be ideal to solve the multi-constrained large-scale power systems.

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INTRODUCTION

Load growth in a power system is increasing faster than the transmission capability. In the past decade, the increase in transmission capability has been almost 50% of the increased generation capability. The transmission system thus faces several challenges. In the extant open-access power system where everybody can sell or buy energy, there is increasing need for improvements in the transmission capacity of the system whereas maintaining system reliability and security (Y.H. Song and X. Wang, 2003).

Due to huge investment for transmission system, determination of loadability limit is an important role for future development of power systems. A loadability limit of power system is related to thermal, voltage stability and security monitoring. It is the margin between the operating point of the system and the maximum loading point. Recently, various techniques are used to determine the maximum loadability limit (G.D. Irisarri *et al.*, 1997), (A. Shunmugalatha and S. Mary Raja Slochanal, 2008), (K. Gnanambal and C.K. Babulal, 2012).

The North American Electrical Reliability Council (NERC) has recognized a structure for formative ATC of interconnected networks (NERC report, 1997). Continuation power flow, repeated power flow based approaches were used by various researchers to determine ATC and TTC (G.C. Ejebe *et al.*, 1998), (V. Ajjarappu and C. Christy, 1992), (Y. Ou and C. Singh, 2002).

During the evaluation of TTC, the system operator needs valuable information regarding the proficiency of an interconnected network to consistently transfer bulk power between two nodes or between different areas of the network without causing threat to system reliability. It has been well demonstrated that the location of the devices and their control parameters significantly affect TTC, which could be overcome with the use of FACTS devices. The capability of the transmission system has improved with FACTS technology (Xiao Ying *et al.*, 2003), (H. Sawhney and B. Jeyasurya 2004), (N.D. Ghawghawe and K.L. Thakre, 2009), (R. Mohan Mathur and Rajiv K. Varma, 2002), (Y. Xiao *et al.*, 2001), (Y. Xiao *et al.*, 2003).

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FACTS devices can offer effective TTC enhancement with low operation and maintenance cost. Several evolutionary algorithms have been used to identify the optimal location and size of FACTS devices. For example, a probabilistic based method was employed for complex and large-scale power systems (M.A. Khaburi and M.R. Haghifam, 2010). A hybrid real-coded genetic algorithm (RCGA) is demonstrated in (T. Nireekshana *et al.*, 2012), and a hybrid mutation particle swarm optimization is demonstrated in (H. Farahmand *et al.*, 2012).

Recently, a biogeography-based optimization (BBO) algorithm was proposed for solving optimization problems (D. Simon, 2008). In this approach, islands or habitats were modeled to represent solutions, and immigration and emigration of species between islands denote sharing of features between solutions. For optimization problems of economic load dispatch in power systems, this method has been tested (A. Bhattacharya and P.K. Chattopadhyay, 2010).

Adaptive real coded biogeography based optimization (ARCBBO) is developed by implementation of adaptive Gaussian mutation with BBO algorithm. Adopting the ARCBBO technique, the paper aims to enhance loadability limit and TTC with the use of FACTS controllers like TCSC and SVC. Active and reactive power control as well as adaptive voltage magnitude control can be regulated simultaneously by ARCBBO. So, this problem is considered as optimal power flow problem (OPF). ARCBBO is used to solve OPF problem and it has been tested on standard 30-bus and IEEE 118-bus systems.

2. Problem Formulation:

ATC is calculated according to the NERC procedure. It is the difference between total transfer capability (TTC) and the sum total of existing transmission commitment (ETC), transmission reliability margin (TRM) and capacity benefit margin (CBM) (NERC report, 1997). TTC is limited by the system characteristics including thermal, voltage and stability limits. ETC is calculated from base case power flow analysis. TRM is usually a constant (i.e. 10% of the TTC). CBM is calculated from the market values of energy contractors. It can be expressed as

$$ATC = TTC - (TRM + CBM + ETC) \quad (1)$$

$$TTC = \text{Minimum}\{\text{Thermal, Voltage, Stability}\} \quad (2)$$

The goal of intensification of TTC is a multi-constrained optimization problem whose solution is expected to find the best location and size of FACTS devices. The objective function is to maximize the system loadability limit and hence TTC is improved. Repeated power flow method is used to solve the following power flow equations.

$$\text{Maximize } f = \sum_{i=1}^{N_{pq}} \lambda_i \quad (3)$$

$$P_{Di} = P_{Di}^0 (1 \pm \lambda_i) \quad (4)$$

$$TTC = \sum_{k \in NL} S_k \quad (5)$$

Subjected to

(i) Power flow constraints

$$P_{Gi} - P_{Di} - \sum_{j=1}^{N_b} V_i V_j [G_{ij} \cos(\delta_i - \delta_j) + B_{ij} \sin(\delta_i - \delta_j)] = 0 \quad i = 1, 2, \dots, N_b \quad (6)$$

$$Q_{Gi} - Q_{Di} - \sum_{j=1}^{N_b} V_i V_j [G_{ij} \sin(\delta_i - \delta_j) - B_{ij} \cos(\delta_i - \delta_j)] = 0 \quad i = 1, 2, \dots, N_b \quad (7)$$

$$P_{Gi}^{\min} \leq P_{Gi} \leq P_{Gi}^{\max} \quad i = 1, 2, \dots, N_g \quad (8)$$

$$Q_{Gi}^{\min} \leq Q_{Gi} \leq Q_{Gi}^{\max} \quad i = 1, 2, \dots, N_g \quad (9)$$

$$V_i^{\min} \leq V_i \leq V_i^{\max} \quad i = 1, 2, \dots, N_{pq} + N_g \quad (10)$$

$$S_k \leq S_k^{\max} \quad (11)$$

where λ_i is the loadability factor for each load bus, P_{Gi} & Q_{Gi} are the active and reactive power injected at bus i , P_{Di} & Q_{Di} are the active and reactive power demand at bus i , V_i & δ_i are the magnitude and phase angle of voltage at bus i , G_{ij} & B_{ij} are the real and imaginary part of admittance of transmission line, N_b , N_g & N_{pq} are the number of bus, number of generator and number of load bus, respectively. S_k is the thermal limit of the k^{th} transmission line. min and max represents the minimum and the maximum limits of the parameter, respectively.

(ii) FACTS device constraints

Here, SVC is used as a reactive power absorption device, as explained in equation (12).

$$Q_{SVC} = B_{SVC} \times (V_{ref}^2) \quad (12)$$

$$-100\text{MVar} \leq Q_{\text{SVC}} \leq 100\text{MVar} \quad (13)$$

$$-0.8X_L \leq X_{\text{TCSC}} \leq 0.2X_L \quad (14)$$

where B_{SVC} is the susceptance added by placing SVC in the bus, X_{TCSC} is the reactance added by placing TCSC, X_L is the reactance of the line where TCSC is connected, and Q_{SVC} is the reactive power injected at the bus by connecting SVC.

Finally, the objective function with all constraints combined for the OPF problem is given by

$$\text{Min } F = G \sum P_{Di} + \sum_{i \in N_g} \lambda_{Pg} (P_{Gi} - P_{Gi}^{\text{lim}})^2 + \sum_{i \in N_g} \lambda_{Qg} (Q_{Gi} - Q_{Gi}^{\text{lim}})^2 + \sum_{i \in N_{pq}} \lambda_V (V_{Li} - V_{Li}^{\text{lim}})^2 + \sum_{i \in NL} \lambda_{Pf} (S_i - S_i^{\text{max}})^2 \quad (15)$$

where G is a constant and λ_{Pg} , λ_{Qg} , λ_V and λ_{Pf} are penalty factors.

3. Review of Biogeography-Based Optimization:

BBO has been proposed by Dan (D. Siman, 2008) as a comprehensive algorithm for solving optimization problems and is based on the study of geographical distribution of species. The BBO approach has two main operators, namely migration operator and mutation operator.

3.1 Migration Operator:

Migration is the process by which each individual in the habitat is probabilistically modified by sharing information with other individual solutions. A geographical area with high habitat suitability index (HSI) is said to be well suitable for biological species. It tends to have a large number of species, high emigration rate, and low immigration rate. Suitability index variables (SIVs) are those that characterize the habitat of the species. Therefore, a habitat with a high HSI tends to be more static in its species distribution. A habitat with a high HSI is analogous to a good solution, and a habitat with a low HSI is analogous to a poor solution. The individuals in a habitat share features based on the migration rate. Immigration rate, λ_k , and emigration rate, μ_k , are functions of the number of species in a habitat. When there are no species in a habitat, its immigration rate is maximum. λ_k can be found by:

$$\lambda_k = I \left(1 - \frac{k}{n} \right) \quad (16)$$

where I is the maximum possible immigration rate, k is the number of species of k th individual, and n is the maximum number of species. μ_k can be found by:

$$\mu_k = E \left(\frac{k}{n} \right) \quad (17)$$

where E is the maximum possible emigration rate.

3.2 Mutation Operator:

Mutation tends to increase the diversity among individuals in a habitat in approaching a better solution. Due to natural events, the HSI of a habitat may change dramatically, resulting in a species count distinct from its equilibrium value. Species count may be associated with a probability value (P_i). If the probability value is very low, an individual's solution is assumed to have been mutated with other solutions. So, mutation rate of individual solution can be calculated using species count probability, given by:

$$M_i = M_{\text{max}} * \left(\frac{1 - P_i}{P_{\text{max}}} \right) \quad (18)$$

where M_i is the mutation rate, M_{max} is the maximum mutation rate, which is a user-defined parameter, and P_{max} is the maximum probability of species count.

4. Adaptive Real-Coded Biogeography-Based Optimization:

In BBO, Migration operator can improve the performance of BBO. It is used to modify habitat by simply replacing similar kind of habitat that means habitat shares less information from the others. Hence, migration operator is lacking of exploration ability.

In order to share more information in between habitats, BBO is inspired with DE, the migration operator is improved by applying DE mutation strategy. The following operation is used as migration operator in this paper, $X_i = X_{\text{best}} + F \times |(X_{r1} - X_{r2})|$ (19)

Where X_i is the i^{th} individual, X_{best} is the best individual, X_{r1} and X_{r2} are the random individuals among the total population and F is the scaling factor.

In BBO, individuals are encoded by a floating point for the continuous optimization problems and random mutation is used which deficient the exploration ability. In RCBBBO (Wenyin Gong *et al.*, 2010), individuals are

represented by a D-dimensional real parameter vector, and a probabilistically based Gaussian mutation operator is used, which improves the diversity of the population and its searching ability.

The Gaussian mutation characteristic function is given by:

$$X_i' = X_i + N(\mu, \sigma_i^2) \quad (20)$$

where $N(\mu, \sigma_i^2)$ represents the Gaussian random variable with mean μ and variance σ^2 . The values of mean and variance are considered 0 and 1, respectively (Wenyin Gong *et al.*, 2010).

Generally, a probability-based mutation operation affects the convergence characteristics. Therefore, adaptive Gaussian mutation is applied in the present work to improve the solution of worst half of individuals in the population. In equation (19), $\mu = 0$, and σ_i is found using the following equation:

$$\sigma_i = \beta * \sum_{i=1}^n \left(\frac{F_i}{f_{\min}} \right) * (X_i^{\max} - X_i^{\min}) \quad (21)$$

where β is the scaling factor or mutation probability, F_i is the fitness value of i th individual, and f_{\min} is the minimum fitness value of the habitat in the population.

Adaptive mutation probability is given by

$$\beta = \beta_{\max} - \frac{\beta_{\max} - \beta_{\min}}{T_{\max}} \times T \quad (22)$$

where $\beta_{\max} = 1$, $\beta_{\min} = 0.005$, T_{\max} is the maximum iteration, and T is the current iteration.

The method of adaptive mutation has the ability to prevent premature convergence and hence to produce a smooth convergence. This method of mutation can be easily used with real-coded variables, which have been widely used in evolutionary programming (EP), and hence to carry out local as well as global searches.

The pseudo code of an ARCBBO algorithm is given below:

Initialize the ARCBBO parameters

Generate the individuals (SIV) randomly within their feasible region

$$X_k = X_k^{\min} + \text{rand}(0,1) \times (X_k^{\max} - X_k^{\min})$$

Calculate the fitness (HSI) value for each habitat in the population

While halting criteria is not satisfied **do**

Sort the SIVs from best to worst according to the fitness value

Map the HSI values to the number of species

Compute immigrate rate and emigration rate for each individual

For $i=1$ to NP

Select X_i according to immigration rate λ_i

For $j=1$ to NP

Generate two integer randomly $r1 \neq r2$

Select X_j according to emigration rate μ_j

If $\text{rand}(0,1) < \mu_j$

$$$X_i = X_j$$$

Else

$$$X_i = X(\text{HSI}_{\text{best}}) + F \times |(X_{r1} - X_{r2})|$$$

End If

End For

End For

// Adaptive Gaussian Mutation (Mutate only the worst half of population)

For $i = (\text{NP}/2) + 1$ to NP

For $j=1$ to N_{var}

$$$\sigma_{ij} = \beta \frac{F_i}{F_{\min}} \times (X_i(j) - X_i(j))$$$

$$$X_{ij}' = X_{ji} + \text{Normrnd}(0, \sigma_{ij})$$$

End For

End For

Compute HSI for new habitats

Sort SIV from best to worst

End While:

Generators active power, system loadability factor for each load bus, FACTS devices location and ratings are the individuals (SIV) of the habitat. Fitness value (HSI) is calculated from objective function, equation (15).

RESULTS AND DISCUSSION

The proposed ARCBBO algorithm is applied to improve the loadability limit and enhance the total transfer capability of system under consideration of with and without FACTS devices. Loadability limit and TTC are calculated under intact case and contingency condition. It has been implemented on the MATPOWER 30-bus and IEEE 118-bus systems and the results are presented here. Power flow calculations by Newton–Raphson method were performed using MATPOWER 4.1 (R.D. Zimmerman *et al.*, 2011).

The optimal control parameters for the algorithm are chosen from number of simulation results. They are: habitat size = 50, habitat modification probability = 1, immigration probability = 1, step size for numerical integration = 1, maximum immigration and emigration rate = 1, mutation probability= 0.005 and maximum number of iterations = 100. The results show the corresponding objective functions for 50 independent trails.

5.1 IEEE 30-bus System:

The system consists of 6 generator buses and 24 load buses. Bus 1 is taken as slack bus. The system load is 189.2 MW and 107.2 MVAR. The details of bus data and line data are taken from MATPOWER package (R.D. Zimmerman *et al.*, 2011). Convergence characteristic of proposed method for 30 bus system is depicted in Fig. 1, which indicates smooth convergence of ARCBBO. For intact case, loadability limits of each load buses are presented in Table 1. Maximum loadability limit obtained for this system by proposed method is compared with different optimization techniques, is presented in Table 2. Loadability limit obtained by the proposed method is 319.3081MW which is better than result reported in (A. Shunmugalatha and S. Mary Raja Slochanal, 2008), (K. Gnanambal and C.K. Babulal, 2012). TTC is calculated by the proposed method with FACTS and without FACTS devices under intact case and contingency condition, results are presented in Table 3.

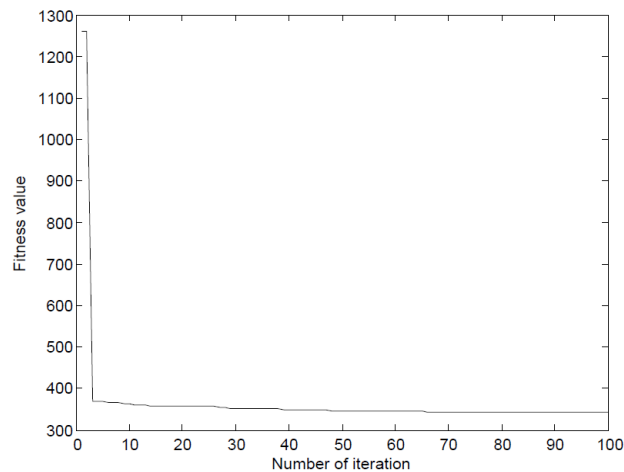


Fig. 1: Convergence characteristics of ARCBBO for 30 bus system.

Table 1: Active power demand at each load buses for 30 bus system.

| Bus No. | Without FACTS | With FACTS | Bus No. | Without FACTS | With FACTS |
|---------|---------------|------------|---------|---------------|------------|
| 3 | 16.9486 | 16.0738 | 16 | 14.5522 | 7.6851 |
| 4 | 25.9129 | 32.1941 | 17 | 4.8770 | 0.2915 |
| 5 | 21.1438 | 22.8444 | 18 | 10.1016 | 0 |
| 6 | 22.2846 | 26.0667 | 19 | 2.4932 | 2.5400 |
| 7 | 6.0826 | 3.5292 | 20 | 11.6741 | 3.7730 |
| 8 | 18.9991 | 21.3314 | 21 | 0 | 4.6822 |
| 9 | 11.9278 | 26.0000 | 24 | 24.9703 | 19.3836 |
| 10 | 0.3365 | 18.5126 | 25 | 4.0056 | 2.4209 |
| 11 | 7.8250 | 11.1130 | 26 | 3.8875 | 6.3852 |
| 12 | 23.1213 | 21.1893 | 28 | 32.1709 | 13.9862 |
| 14 | 1.4763 | 4.4651 | 29 | 17.3830 | 13.3354 |
| 15 | 6.1937 | 10.1522 | 30 | 6.0409 | 13.2127 |

Table 2: Comparison of maximum loadability in MW.

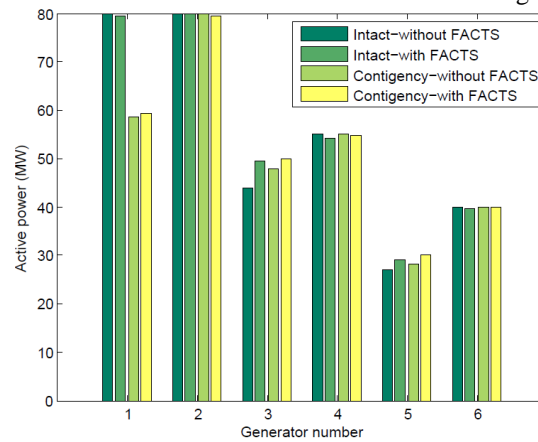
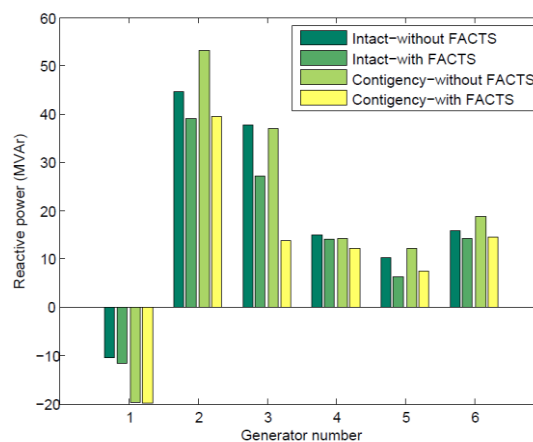
| System | ARCBBO(with FACTS) | ARCBBO(without FACTS) | DEPSO (K. Gnanambal and C.K. Babulal, 2012) | DE (K. Gnanambal and C.K. Babulal, 2012) | MAHPSO (A. Shunmugalatha and S. Mary Raja Slochanal, 2008) |
|---------|--------------------|-----------------------|---|--|--|
| 30 bus | 326.0674 | 319.3081 | 269.74 | 267.09 | 260.808 |
| 118 bus | 7892.3 | 7855.9 | 5701.56 | 5654.3 | 5645 |

Table 3: Enhancement of TTC for 30 bus system.

| Case | Loadability (MW) | TTC (MVA) | SVC | | TCSC | | Limiting point |
|---------------------------|------------------|-----------|--------------|-----------------|---------------|-----------------------|----------------------|
| | | | Bus location | Capacity (MVAR) | Line location | Level of compensation | |
| Intact without FACTS | 319.3081 | 621.4888 | - | - | - | - | Line flow at line 29 |
| Intact with FACTS | 326.0674 | 632.5870 | 11 | 23.0337 | 28 | 0.2285 | Line flow at line 29 |
| Contingency without FACTS | 302.8279 | 577.6207 | - | - | - | - | Line flow at line 30 |
| Contingency with FACTS | 307.1221 | 633.2993 | 9 | 48.7606 | 15 | 0.0294 | Line flow at line 30 |

Under intact case, network TTC are being 621.4888 MVA and 632.5870 MVA without and with FACTS devices respectively. So network TTC is improved by 11 MVA, connecting SVC at bus 11 and TCSC at line 28. Enhancement of TTC is limited by the system thermal limit, at line 29.

Under contingency condition (line no. 2 is outage); network TTC is 577.6207MVA which is lesser than TTC in intact case. TTC is improved to 633.2993MVA, by connecting SVC at bus 9 and TCSC at line 15. TTC is limited by the system thermal limit, at line 29. Power flow constraints of generator active power, reactive power, bus voltages and line flows are within the limits which are shown in Fig. 2 to 5 respectively.

**Fig. 2:** Generator active power output for 30 bus system.**Fig. 3:** Generator reactive power output for 30 bus system.

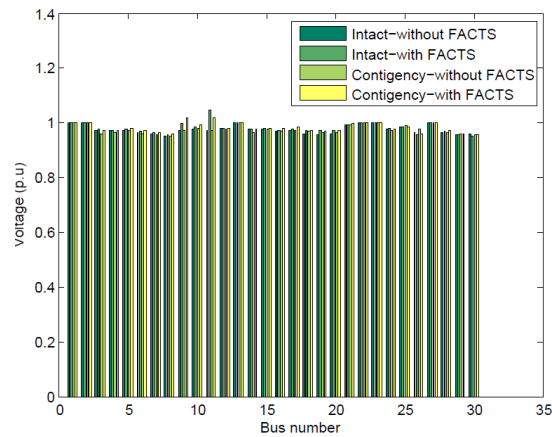


Fig. 4: Bus voltages for 30 bus system.

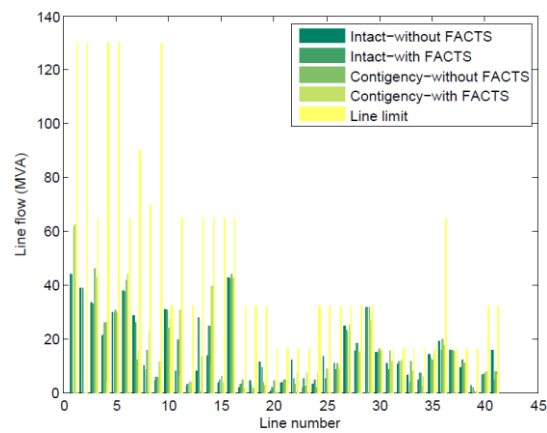


Fig. 5: Line flow for 30 bus system.

5.2 IEEE 118-bus System:

The system consists of 54 generators, 64 load buses, and 186 transmission lines. The system load is 4242 MW and 1438 MVAR. Bus 69 is taken as slack bus. Details of bus data and line data are available in MATPOWER (R.D. Zimmerman *et al.*, 2011). Convergence characteristic of proposed method for IEEE 118-bus system is depicted in Fig. 4. For intact case, loadability limits of each load buses are presented in Table 4. Maximum loadability limit obtained for this system by proposed method is compared with different optimization techniques, is presented in Table 2. Loadability limit obtained by the proposed method is 7855.9MW which is better than result reported in (A. Shunmugalatha and S. Mary Raja Slochanal, 2008), (K. Gnanambal and C.K. Babulal, 2012).

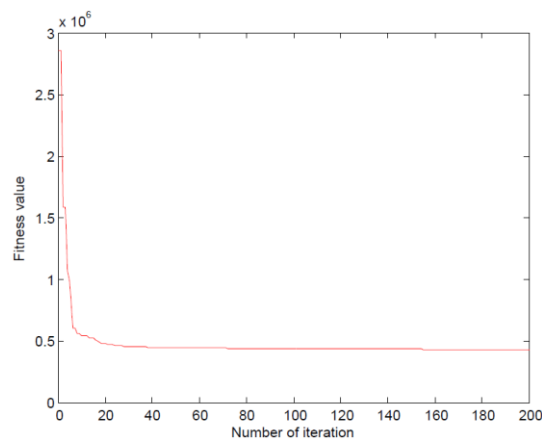


Fig. 6: Convergence characteristics of RCBBO for 118 bus system.

Table 4: Active power demand at each load buses for 118 bus system.

| Bus No. | Without FACTS | With FACTS | Bus No. | Without FACTS | With FACTS |
|---------|---------------|------------|---------|---------------|------------|
| 2 | 23.0586 | 79.9044 | 57 | 81.3289 | 45.4217 |
| 3 | 98.1735 | 96.9886 | 58 | 79.2579 | 43.4419 |
| 5 | 96.3530 | 86.8049 | 60 | 100.0000 | 96.6523 |
| 7 | 100.0000 | 99.9005 | 63 | 100.0000 | 95.9065 |
| 9 | 83.5788 | 78.0128 | 64 | 100.0000 | 94.3537 |
| 11 | 80.3167 | 85.8058 | 67 | 99.1669 | 100.0000 |
| 13 | 53.9803 | 75.3256 | 68 | 82.9532 | 89.0645 |
| 14 | 33.6117 | 89.5740 | 71 | 99.2755 | 98.6430 |
| 16 | 72.7967 | 48.3855 | 75 | 99.6552 | 98.0307 |
| 17 | 98.9483 | 95.0239 | 78 | 99.1639 | 73.1352 |
| 20 | 33.0375 | 63.0651 | 79 | 96.5270 | 100.0000 |
| 21 | 21.1931 | 4.7420 | 81 | 60.5157 | 93.8465 |
| 22 | 43.2734 | 15.5592 | 82 | 99.1433 | 84.7319 |
| 23 | 98.6558 | 80.9256 | 83 | 51.0489 | 77.0457 |
| 28 | 99.2395 | 99.3429 | 84 | 84.7483 | 64.9145 |
| 29 | 93.3293 | 97.0154 | 86 | 73.2564 | 97.0659 |
| 30 | 100.0000 | 98.2078 | 88 | 85.5662 | 86.3975 |
| 33 | 65.1049 | 89.8368 | 93 | 39.2316 | 96.5508 |
| 35 | 99.9795 | 95.6184 | 94 | 67.8757 | 91.8598 |
| 37 | 87.5565 | 97.0489 | 95 | 71.3100 | 96.1851 |
| 38 | 100.0000 | 83.4558 | 96 | 90.8709 | 85.2284 |
| 39 | 83.1275 | 99.8287 | 97 | 99.6233 | 99.7388 |
| 41 | 100.0000 | 85.3500 | 98 | 91.0107 | 99.2103 |
| 43 | 43.8970 | 62.4266 | 101 | 84.5546 | 78.3387 |
| 44 | 70.3243 | 63.4835 | 102 | 81.6207 | 80.5135 |
| 45 | 100.0000 | 59.1034 | 106 | 82.6082 | 96.7077 |
| 47 | 91.1520 | 98.1230 | 108 | 98.1115 | 66.3685 |
| 48 | 99.3886 | 100.0000 | 109 | 71.6877 | 95.4820 |
| 50 | 100.0000 | 50.2750 | 114 | 90.3965 | 97.6445 |
| 51 | 16.8021 | 16.4511 | 115 | 98.9341 | 99.5025 |
| 52 | 37.2497 | 28.5217 | 117 | 66.5761 | 3.3476 |
| 53 | 17.5923 | 34.2051 | 118 | 79.1353 | 99.6629 |

TTC is calculated by the proposed method with FACTS and without FACTS devices under intact case and contingency condition, results are presented in Table 5. Network TTC are 12947 MVA (without FACTS) and 13051 MVA (with FACTS) under intact case where TTC is limited by system voltage limit at bus 108 and 109 respectively. TTC is improved by connecting SVCs at buses 49 & 77 and TCSCs at lines 174 & 184.

Under contingency condition (transformer connected in line 5-8 is outage), network TTC is 12710 MVA (without FACTS) and 13335 MVA (with FACTS). TTC is improved by 5%, connecting SVCs at buses 45 & 51 and TCSC at lines 145 & 184. Power flow constraints of generator active power, reactive power and bus voltages are within the limits which are shown in Fig. 7 to 9 respectively.

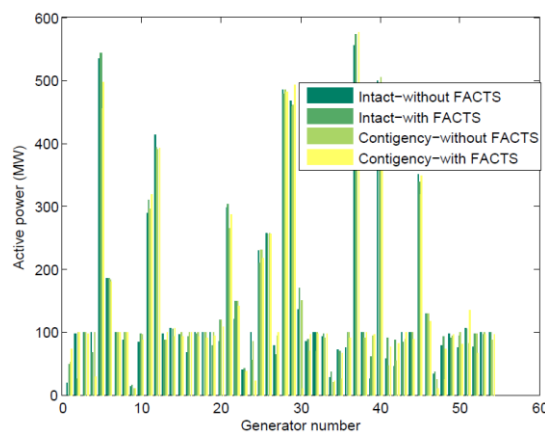


Fig. 7: Generator active power output for 118 bus system.

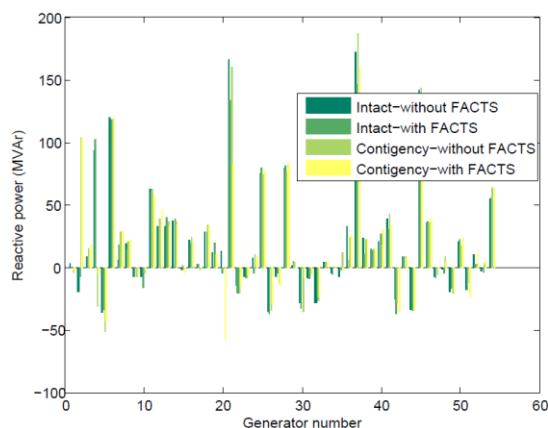


Fig. 8: Generator reactive power output for 118 bus system.

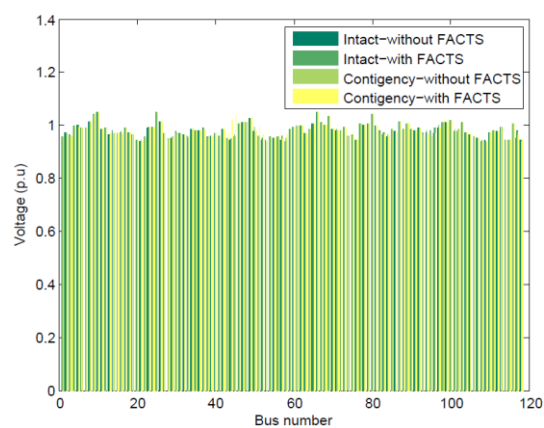


Fig. 9: Bus voltages for 118 bus system.

Table 5: Enhancement of TTC for 118 bus system.

| Case | Loadability (MW) | TTC (MVA) | SVC | | TCSC | | Limiting point |
|---------------------------|------------------|-----------|--------------|------------------|---------------|-----------------------|--------------------|
| | | | Bus location | Capacity (MVAR) | Line location | Level of compensation | |
| Intact without FACTS | 7855.9 | 12947 | - | - | - | - | Voltage at bus 108 |
| Intact with FACTS | 7892.3 | 13051 | 95,96 | 54.5651, 38.8503 | 141, 169 | 0.6,0.6 | Voltage at bus 109 |
| Contingency without FACTS | 7644.7 | 12710 | - | - | - | - | Voltage at bus 57 |
| Contingency with FACTS | 7674.7 | 13335 | 51,45 | 98.9971, 95.6895 | 145, 184 | 0.6,0.065 | Voltage at bus 21 |

6. Conclusion:

In this paper, ARCBBO algorithm was successfully applied to OPF based enhancement of loadability limit and TTC of the power system. This algorithm is tested to be efficient in identifying the optimal location and size of FACTS devices for improvement of TTC in standard 30-bus and IEEE 118-bus systems under intact and contingency conditions. The solution quality of the proposed method is superior over other techniques reported in recent literature. This solution is very useful to independent system operator (ISO) in deregulated power system, because enhancement of total transfer capability may be used for future transaction in transmission system, against the investment of new transmission lines. Due to its simple framework, and smooth and quick convergence characteristics, the ARCBBO algorithm is suggested to be ideal to solve the multi-constrained large-scale power systems.

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